

Consideration Spectroscopy Characterization and Influence of Cooperative Up-Conversion in Erbium Doped Ta_2O_5 Trapezoid Waveguide Amplifier

Golnoosh Mesri, Mohammad Mohebbi

Department Of Electronic, Qazvin Branch, Islamic Azad University, Qazvin, Iran.

Corresponding Email : Golnooshmesri@gmail.com

Abstract:

We report the design and simulation of spectroscopic characteristics and gain of erbium doped Ta_2O_5 trapezoid waveguide amplifier. Guiding modes, field distribution are calculated. Percentage of core power at wavelength of $1.53\mu m$, $0.98\mu m$ and overlap factor studied. Based on rate equation, influence of cooperative up-conversion on gain with consideration to different parameters is numerically calculated.

Keywords:

Erbium, Gain, Tantalum pentoxide, Waveguide amplifier.

I. Introduction

Erbium doped waveguide amplifiers (EDWA) are key components in optical telecommunications. EDWA can provide high gain and in a variety of hosts have been developed rapidly. Especially Ta_2O_5 waveguide amplifiers on SiO_2 substrate have attracted considerable attention. Ta_2O_5 is chosen as host material of erbium, which is a high refractive index material and having a refractive index greater than 2[i]. On the other hand high confinement can be realized with large refractive index changes between Ta_2O_5 and SiO_2 . Tantalum pentoxide had high radiative efficiency and a large third order non-linearity [ii,iii]. A high refractive index contrast material allows strong confinement of light. Optical amplifiers have low propagation losses. Optical measurements were calculated yield the waveguide attenuation and erbium absorption and emission cross-section. Spectroscopy and performance of erbium doped Ta_2O_5 rectangular waveguide amplifiers were calculated [iv]. In this paper we report the characteristics of erbium doped Ta_2O_5 trapezoid waveguide amplifier. We analyze the influence of etched cross-section on guiding modes, field distribution, mode intensity and overlap factor between signal and pump wavelengths.

Finally we calculated gain of waveguide amplifier and represented effect of cooperative up-conversion.

II. Experimental procedures

In this article trapezoid waveguide amplifier is considered with width of $w_1=2\mu m$, $w_2=0.4\mu m$, rib height $h=1\mu m$ and etch depth of $D=0.3\mu m$, as shown in Fig. 1(a). The refractive index of core and cladding are 2.1 and 1.44 respectively.

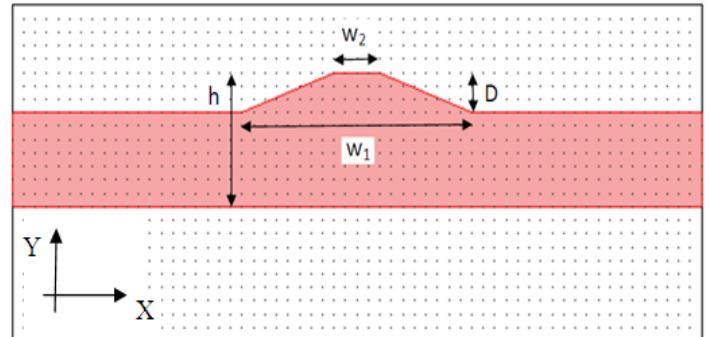
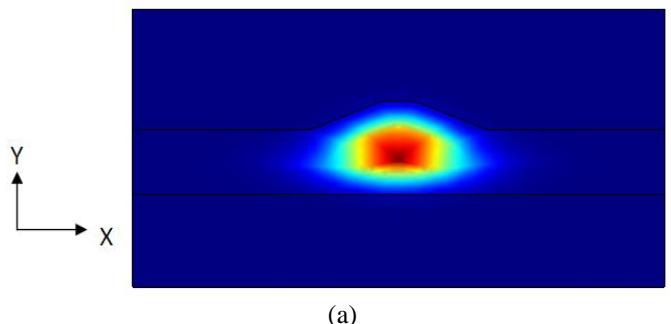
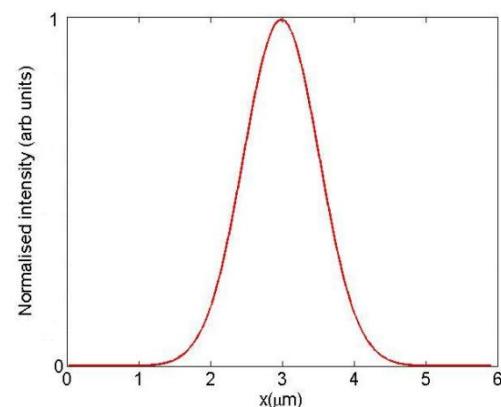


Fig. 1. Schematic diagram of the rib trapezoid waveguide with dimension of $w_1=2\mu m$, $w_2=0.4\mu m$, $D=0.3\mu m$ and $h=1\mu m$.

Guiding modes and field distribution and intensity of the mode overlap factor with the active region in the above waveguide are analyzed by COMSOL Multiphysics Software for the signal(1530nm) and pump(980nm) wavelengths shown in fig 2.



(a)



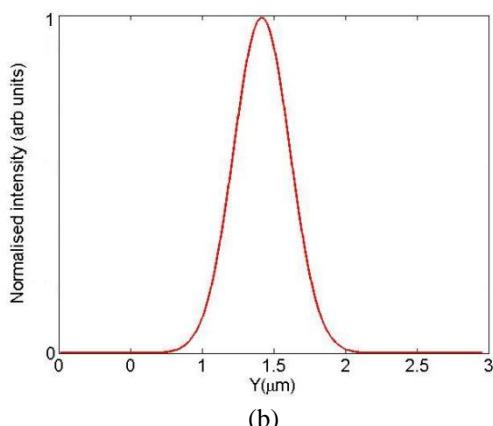


Fig. 2: (a) Simulation of mode profile for the trapezoid waveguide at signal and pump wavelengths. (b) Mode intensity profile in the x and y directions.

II. Results and discussion

Gain measurements were performed by solving the rate equations for the erbium ions in a three-level erbium ion system with the pump and signal evolution along the length of the waveguide in MATLAB software. If n_1 , n_2 and n_3 be the fraction of population of the erbium ions and N_t be the total erbium concentration, then the following can be written

$$\frac{dn_1}{dt} = -W_{13}n_1 + W_{21}n_2 - W_{12}n_1 + \frac{n_2}{\tau_{21}} + N_t C_{up} n_2^2 \quad (1)$$

$$\frac{dn_2}{dt} = W_{12}n_1 - W_{21}n_2 - \frac{n_2}{\tau_{21}} - 2N_t C_{up} n_2^2 + \frac{n_3}{\tau_{32}} \quad (2)$$

$$\frac{dn_3}{dt} = W_{13}n_1 + N_t C_{up} n_2^2 + \frac{n_3}{\tau_{32}} \quad (3)$$

$$W_{ij} = \frac{I_{p,s} \sigma_{i,j}^{p,s}}{h \nu_{p,s}} \quad (4)$$

In these equations, the W_{ij} terms represent the stimulated transition rates between the i and j levels. $I_{p,s}$ is the pump and signal intensities. The evolution of signal and pump powers along the propagation direction is governed by the following differential equations:

$$\frac{dp_p(z)}{dz} = (-\alpha_p + (\sigma_{31}n_3(z) - \sigma_{13}n_1(z))\Gamma_p N_t)P_p(z, \nu_p) \quad (5)$$

$$\frac{dp_s(z)}{dz} = (-\alpha_s + (\sigma_{21}n_2(z) - \sigma_{12}n_1(z))\Gamma_s N_t)P_s(z, \nu_s) \quad (6)$$

$$G(z) = (dP_s/dz)/P_s(z) = (-\alpha_s + (\sigma_{21}n_2(z) - \sigma_{12}n_1(z))\Gamma_s N_t) \quad (7)$$

$G(z)$ is the gain of the amplifier. The parameters used for evaluate the gain are shown in **Table 1**.

Table 1: Parameter used in the simulation of signal gain [iv].

parameter	value
(σ_{12}) signal absorption cross section at 1527nm	$4.8 \times 10^{-21} \text{ cm}^2$
(σ_{21}) signal emission cross section at 1527nm	$4.4 \times 10^{-21} \text{ cm}^2$
(σ_{13}) pump absorption cross section at 977nm	$2.1 \times 10^{-21} \text{ cm}^2$
(σ_{31}) pump emission cross section at 977nm	0 cm^2
(τ_{21}) lifetime $I_{13/2}$	2.3 ms
(τ_{32}) lifetime $I_{11/2}$	$30 \mu\text{s}$
(α_p) waveguide loss at pump wavelength	0.23 cm^{-1}
(α_s) waveguide loss at signal wavelength	0.15 cm^{-1}
(Γ_s) overlap factor	0.98
(Γ_p) overlap factor	0.9
(C_{up}) cooperative up-conversion coefficient	$0 - 10^{-17} \text{ cm}^3/\text{s}$

Fig 3 shows the effect of up-conversion on the gain along the length of the waveguide at constant pump power 200 mW and erbium concentration $N_t = 2 \times 10^{20} \text{ ions/cm}^3$, and different C_{up} . At 200 mW with no up-conversion, a high level of inversion is achieved leading to higher gain (28 dB) over the length of 10cm as shown by the blue line in Fig 3. At $C_{up}=1 \times 10^{-18} \text{ cm}^3/\text{s}$ and $C_{up}=1 \times 10^{-17} \text{ cm}^3/\text{s}$ gain is reduced to 27dB and 21dB respectively.

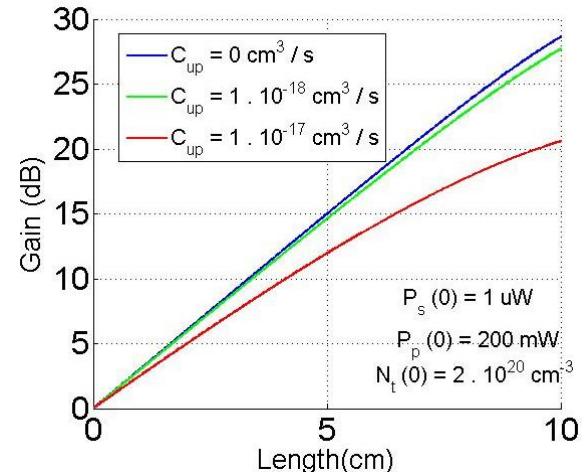


Fig. 3. variation of signal gain along the length of the trapezoid waveguide for fixed erbium concentration, pump and signal power and various up-conversion coefficients.

Fig.4(a, b) shows the gain as a function of erbium concentration with and without up-conversion. This gain was plotted against the erbium concentration at different pump power (10, 100, 200mW) as shown in Fig. 4a. It can be seen from this plot that there does not exist any optimum concentration for any of the three pump powers for maximizing the signal gain from the amplifier. This is because the up-conversion factor has not been taken into account resulting in the increase in the gain with the erbium concentration. Optimum power pump achieved 200mW. In Fig. 4b, the same result is plotted with different C_{up} and the effect of up-conversion can be immediately seen as there is an optimum concentration for achieving maximum gain, at fixed 200mW pump and 1μW signal power.

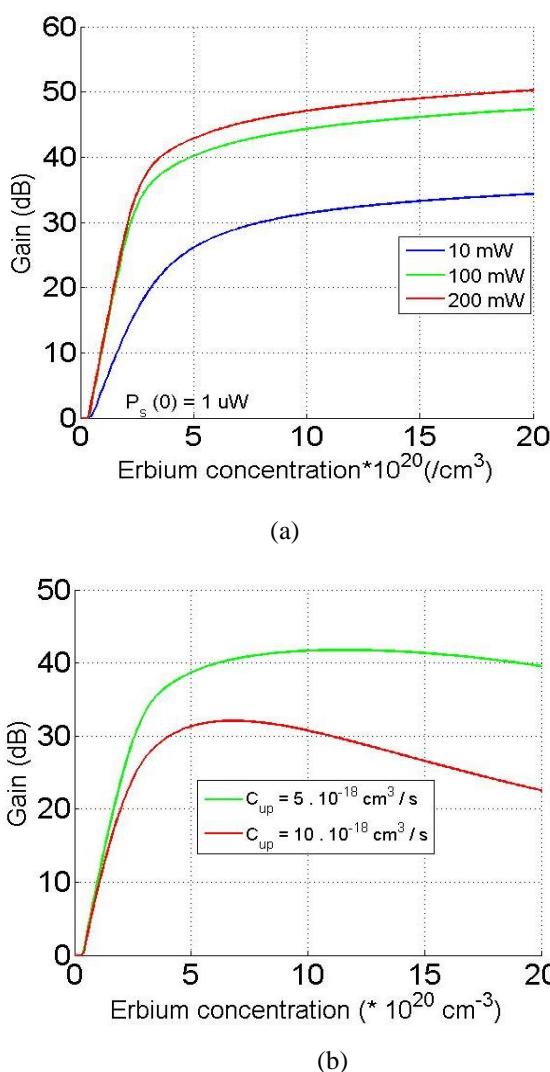


Table.2: Maximum gain achievable in Er:Ta₂O₅ for a pump power of 200mW for different cooperative up-conversion coefficient.

$C_{\text{up}} (\text{cm}^3/\text{s})$	$N_t (\text{ions}/\text{cm}^3)$	Gain(dB)
5×10^{-18}	10×10^{20}	43
10×10^{-18}	7×10^{20}	33

III. Conclusion

The trapezoid waveguide designed in order to obtain higher gain performance and ensure single mode operation at the signal and pump wavelength. Spectroscopic characteristics of waveguide amplifiers are discussed. Reaches well confinement of the electromagnetic field and high overlap factor on the condition of ensuring single mode operation at the signal and pump wavelength. The effect of different up-conversion has been taken into account and its effect on the gain of the system has been represented. The equations were solved numerically and the evolution of signal, pump and gain were obtained by solving the rate equation at each length interval. The signal gain characteristics were analysed as a function of length of the waveguide and erbium concentration.

References

- i. Subramanian A.Z. Oton C.J. Shepherd D.P. Wilkinson J.S. Erbium-doped waveguide laser in tantalum pentoxide. *IEEE Photon. Technology. Lett.*, 2010; 22: 1571-1573.
- ii. Dobal P.S. Katiyar R.S. Jiang Y. Guo R. Bhalla A.S. Raman scattering study of a phase transition in tantalum pentoxide. *J. Raman Spectrosc.* 2000; 31: 1061-1065.
- iii. Tai C.Y. Wilkinson J.S. Perney N.M.B. Netti M.C. Cattaneo F. Finlayson C.E. Baumberg J.J. Determination of nonlinear refractive index in a Ta₂O₅ rib waveguide using self-phase modulation. *Opt. Exp.* 2004; 12: 5110-5116.
- iv. Subramanian A.Z. Murugan G.S. Zervas M.N. Wilkinson J.S. Spectroscopy, modeling and performance of erbium doped Ta₂O₅ waveguide amplifiers. *IEEE*, 2012; 30: 1455-1462.

Fig. 4. Signal gain variation for different erbium concentrations.
 (a) without up-conversion($C_{\text{up}}=0$) and various pump power(10, 100, 200mW). (b) for $C_{\text{up}}=5 \times 10^{-18} \text{ cm}^3/\text{s}$, $C_{\text{up}}=10 \times 10^{-18} \text{ cm}^3/\text{s}$ at optimum pump power 200mW.

This result presented in Fig. 4 is the last and the most important of the performance maps for extracting the optimum performance from the EDWA. The results can be used to predict the erbium concentration and the length of the waveguide for a given pump power and up-conversion coefficient that should be used to extract maximum gain from the amplifier. For Er:Ta₂O₅, for a pump power of 200mW, and signal power of 1 μW , the maximum gain that can be extracted is summarized in Table 2 and is extracted from Fig. 4b. A maximum gain of 43 dB can be achieved at erbium concentration $10 \times 10^{20} \text{ ions}/\text{cm}^3$ and $C_{\text{up}}=5 \times 10^{-18} \text{ cm}^3/\text{s}$. For a very high value of $C_{\text{up}}=10 \times 10^{-18} \text{ cm}^3/\text{s}$, the gain reduces to 33 dB at a reduced concentration of $7 \times 10^{20} \text{ ions}/\text{cm}^3$.